

Design a force platform for measuring center of pressure (COP) signal

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Introduction

- Falls are a major public health concern issue for the elderly people.
- The “**complexity**” was used to reflect adaptability and to determine balance stability from the center of pressure (COP) signals (Costa *et al.*, 2003).
- Application of subsensory noise to the feet has been demonstrated to improve postural stability in the elderly (Costa *et al.*, 2007).
- It is assumed that elderly people can effectively enhance individual’s postural balance stability through plantar vibratory stimulation.
- Main objective is to compare the complexities of COP signals before and after using vibratory insoles for elderly and young adults.

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Noise and poise: Enhancement of postural complexity in the elderly with a stochastic-resonance-based therapy

M. COSTA¹, A. A. PRIPLATA^{2,3}, L. A. LIPSITZ², Z. WU⁴, N. E. HUANG⁵, A. L. GOLDBERGER¹ and C.-K. PENG¹

M. Costa *et al.*

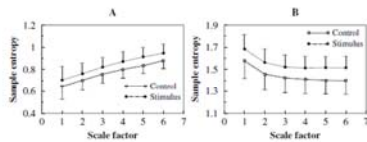


Fig. 2. MSE analysis of: A) anteroposterior and B) mediolateral postural displacement away time series recorded under free-running (control) conditions and with subsensory noise stimulation (stimulus) from a healthy elderly subjects. Time series were detrended using the empirical mode decomposition method. The symbols represent mean values of sample entropy (SampEn) for all subjects and all trials and error bars represent standard errors. Parameters for the calculation of SampEn were: $m = 2$ and $r = 0.15$.

Effect of step-synchronized vibration stimulation of soles on gait in Parkinson's disease: a pilot study

Peter Novak¹ and Vera Novak²

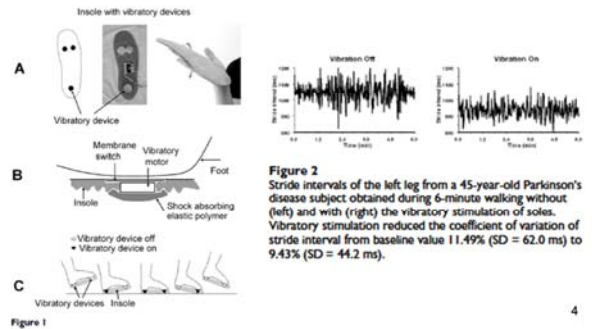


Figure 2. Stride intervals of the left leg from a 45-year-old Parkinson's disease subject obtained during 6-minute walking without (left) and with (right) the vibratory stimulation of soles. Vibratory stimulation reduced the coefficient of variation of stride interval from baseline value 11.49% (SD = 62.0 ms) to 9.43% (SD = 44.2 ms).

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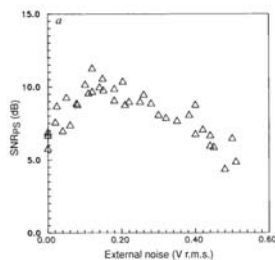
Nature in 1993, Crayfish

Noise enhancement of information transfer in crayfish mechanoreceptors by stochastic resonance

John K. Douglass¹, Lon Wilkens², Eleni Pantazelou¹ & Frank Moss^{1†§}

Departments of ¹ Biology and ² Physics, University of Missouri at St. Louis, St. Louis, Missouri 63121, USA

In linear information theory, electrical engineering and neurobiology, random noise has traditionally been viewed as a detriment to information transmission. Stochastic resonance (SR) is a non-linear, statistical dynamics whereby information flow in a multi-state system is enhanced by the presence of optimized, random noise^{1,2}. A major consequence of SR for signal reception is that it makes possible substantial improvements in the detection of weak periodic signals. Although SR has recently been demonstrated in several artificial physical systems³⁻⁶, it may also occur naturally, and an intriguing possibility is that biological systems have evolved the capability to exploit SR by optimizing endogenous sources of noise. Sensory systems are an obvious place to look for SR, as they excel at detecting weak signals in a noisy environment. Here we demonstrate SR using external noise applied to crayfish mechanoreceptor cells. Our results show that individual neurons can provide a physiological substrate for SR in sensory systems.



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Nature in 1996, Noise-enhanced Tactile Sensation

Noise-enhanced tactile sensation

SIR — Stochastic resonance, a phenomenon in which noise enhances the response of a nonlinear system to a weak signal^{1,2}, has been demonstrated to be important functionally in various physiological systems³⁻⁶. Here we demonstrate improvements in human sensory perception mediated by stochastic resonance-type effects. We show that the ability of an individual to detect a subthreshold tactile

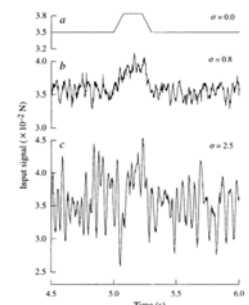
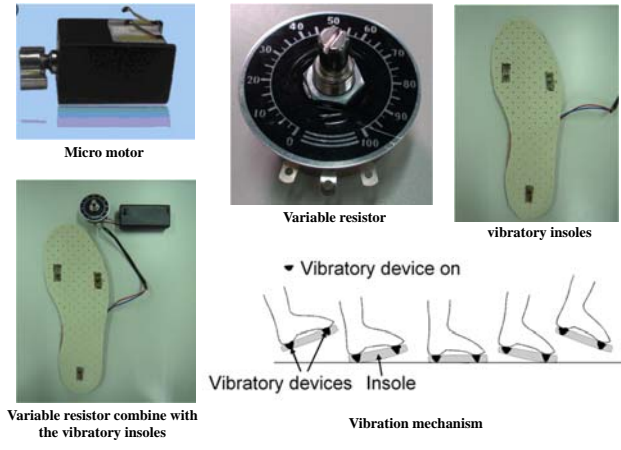
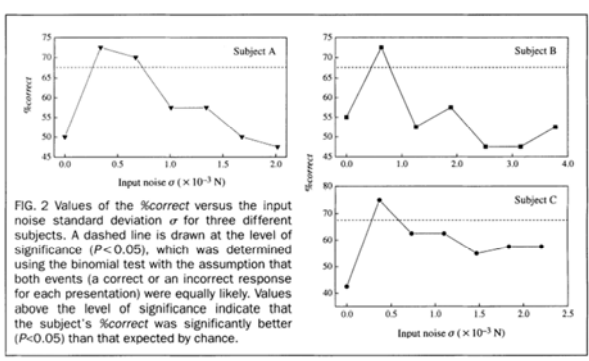


FIG. 1. Representative samples of the input signal for three experimental conditions: a, stimulus with no input noise; b, stimulus with input noise of moderate intensity; c, stimulus with input noise of high intensity. (Respective values for the

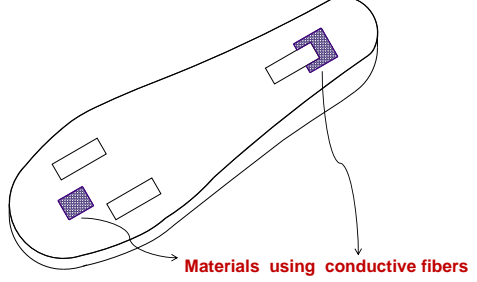
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Part I Design A Balance Stability Enhancement System

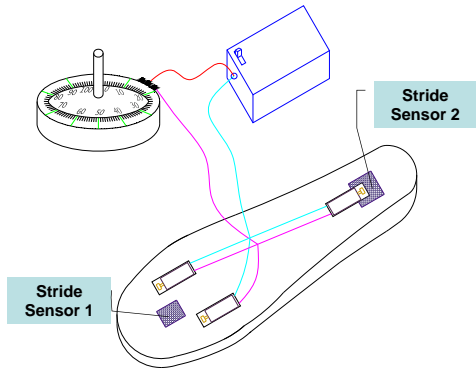


Stride-interval measurement using conductive material

Self-made stride sensors

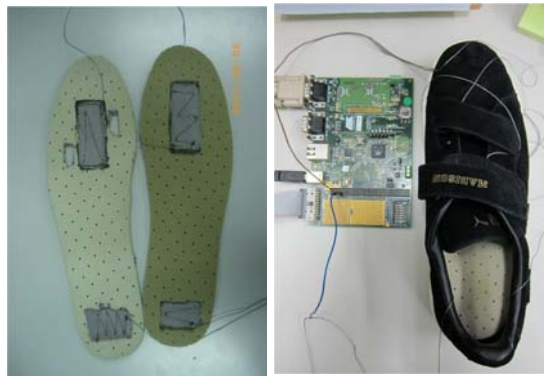


Self-Made Micromotors plus Stride sensors



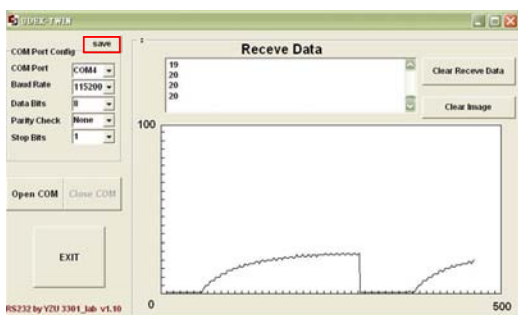
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Self-Made Stride sensors in insole and shoes with ARM



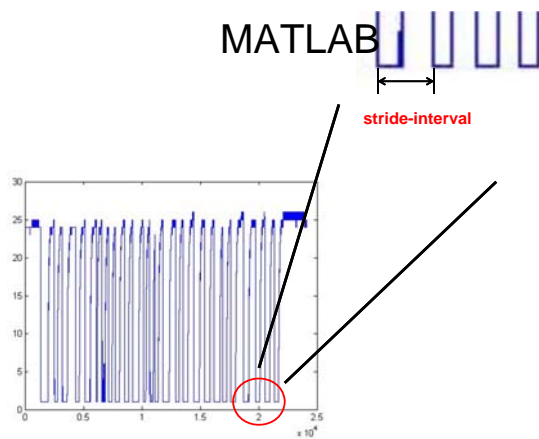
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ARM collecting data



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MATLAB



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Stride-interval measurement using tri-axis accelerometer

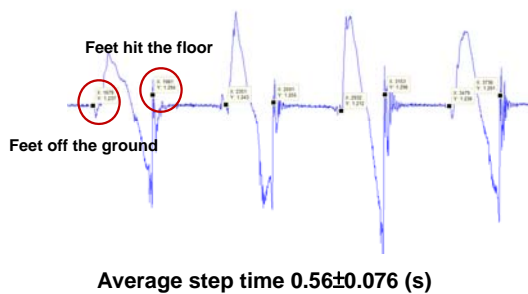


Accelerometer

A/D card (500hz)

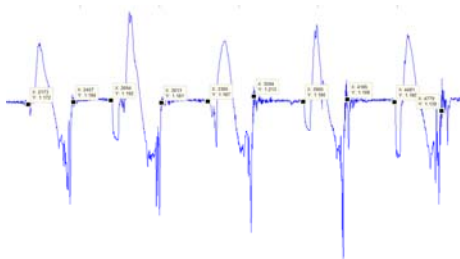
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Step spacing - 30cm



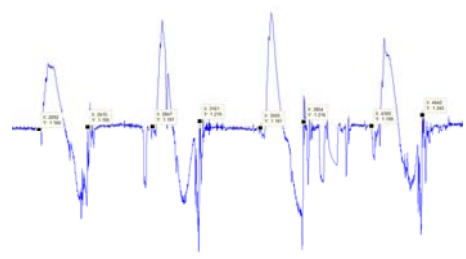
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Step spacing - 40cm



Average step time 0.58 ± 0.054 (s)

Step spacing - 50cm



Average step time 0.63 ± 0.04 (s)

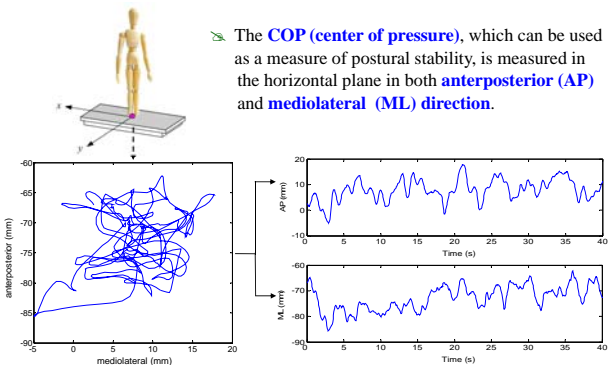
COP force plate

Part II
Multi-Scale Entropy Applied in Fall-Risk
Evaluation via Measuring Non-invasive
Physiologic Signals

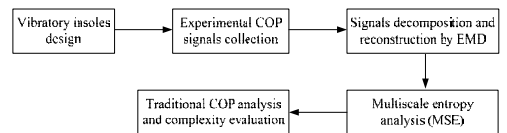
The COP signals were obtained from a force plate CATSYS 2000 (Danish Product Development Ltd., Snekkersten, Denmark) and its signal sampling frequency was about **40Hz**.



Postural stability and COP signal



A functional module flowchart for COP signal analysis



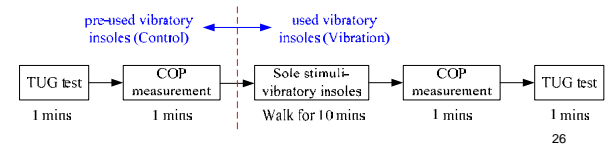
- ✓ EMD technique was adopted to decompose the COP signals.
- ✓ The reconstructed signals were analyzed by MSE.
- ✓ Complexity was evaluated and compared.

Vibratory insoles for elderly and young subjects

- Subjects :
 - 26 elderly subjects (with fall experiences in one year; all males; age range: 65-95 years old).
 - 16 healthy young subjects (fourteen males and two females; age range: 20-30 year old).

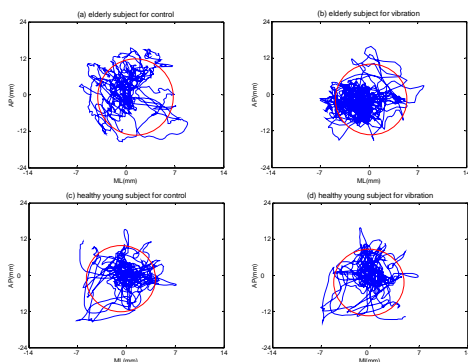
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Time up and go and COP measure experiment



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Traditional COP analysis-Area based

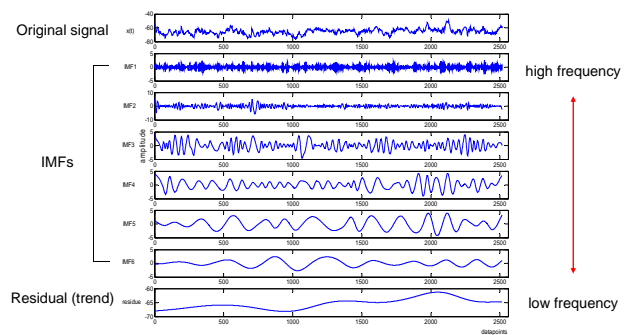


The AREA-CC (95%) can not effectively distinguish the differences in this experiment.

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Empirical mode decomposition (EMD)

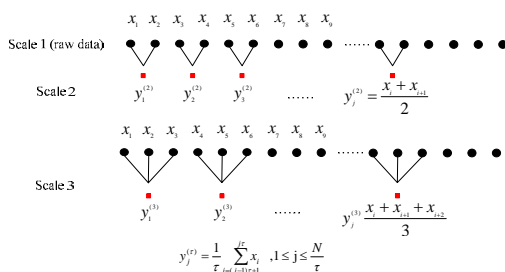
- Huang *et al.* (1998) developed EMD procedure.
- Signal is decomposed into **intrinsic mode functions (IMFs)** by EMD.



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Multi-scale entropy (MSE)

Schematic illustration of the MSE for scale 2 and 3 (Costa *et al.* 2002)



- The entropy is calculated by **sample entropy**.
- Match point (m) and tolerance ratio (r) $\rightarrow m = 2$ and $r = 0.15$

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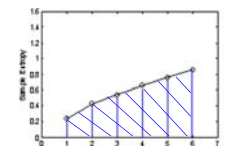
Complexity index (CI)

MSE

- Complexity index (CI) was defined as the area under the MSE curve as

$$CI = \sum_{i=1}^{sn} SampEn(i)$$

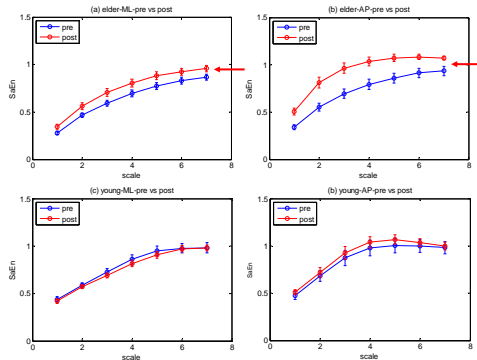
where sn is presented scale numbers.



- CI is compare to determine the complex degree of the signal.
- If the CI value of the subject is greater , the Complexity of the subject is higher.**

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The MSE analysis of reconstructed COP signal (IMF2+IMF3)-EMD



The comparisons of Area-based and MSE for elderly and young subjects under pre-test and post-test conditions

Stabilometric parameters	Elderly fallers		Healthy young		P_a	P_b
	pre	post	pre	post		
Area-based						
AREA-CC (95%) (mm ²)	31.55 ± 14.57	25.11 ± 16.90	25.81 ± 17.53	23.52 ± 13.41	0.104	0.611
AREA-SW (mm ² /s)	58.15 ± 28.13	46.12 ± 22.37	27.7 ± 14.8	23.6 ± 14.31	0.102	0.335
MSE-ML (complexity)	5.205 ± 1.085	5.829 ± 1.353	5.517 ± 0.728	5.349 ± 0.646	0.030	0.427
MSE-AP (complexity)	5.611 ± 0.734	7.263 ± 1.355	5.926 ± 1.266	6.299 ± 0.599	0.001	0.321

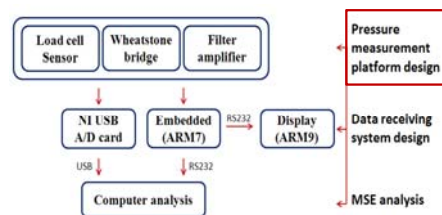
P_a : p-value for elderly subjects between pre-test and post-test.
 P_b : p-value for healthy young subjects between pre-test and post-test.

The statistical significance of MSE-ML and MSE-AP is higher, especially for MSE-AP. ($P_a < 0.001$)

Part III Developing a Fall-Risk Evaluation System

Balance Measurement Device

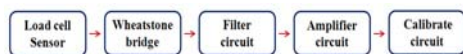
There are many commercial COP measurement systems (such as Kistler, CATSYS2000) in the market. However, their prices are usually too high to be affordable.



The balance measurement system design flow chart

Balance Measurement Device

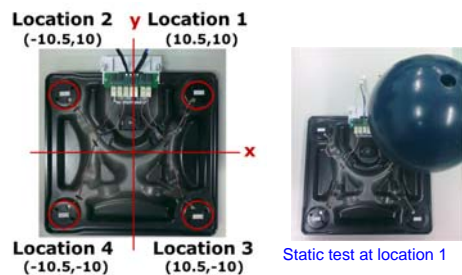
Pressure measurement platform design



Pressure measurement platform

Reproducibility tests

Static state COP test
The location of four static test points



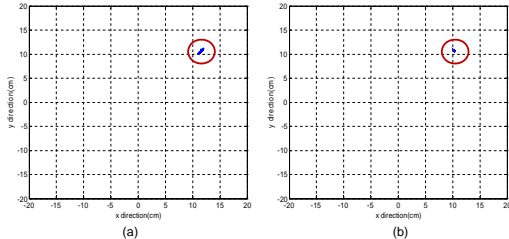
Static test at location 1

Reproducibility tests

Static state COP test

The location of four static test points

Static test at location 1



High resolution balance measurement system

Embedded balance measurement system

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Reproducibility tests

Static state COP test

Result

Table 1. The mean and standard deviation value of four locations which measured by high resolution balance measurement system

	Location 1		Location 2		Location 3		Location 4	
	X	Y	X	Y	X	Y	X	Y
1	-11.325	10.401	-10.428	9.9516	12.219	-11.020	-11.249	-10.618
2	11.292	10.35	-11.087	10.363	12.373	-11.188	-11.747	-11.084
3	-11.277	10.326	-11.051	10.412	12.440	-11.263	-11.124	-10.548
4	11.335	10.373	-11.105	10.521	12.104	-10.925	-11.402	-10.759
5	11.272	10.306	-10.925	10.371	12.125	-10.944	-11.257	-10.667
6	11.495	10.516	-10.739	10.233	12.111	-10.936	-10.856	-10.301
7	11.428	10.459	-10.926	10.384	12.108	-10.935	-11.082	-10.515
8	11.433	10.46	-10.688	10.183	12.036	-10.881	-11.253	-10.667
9	11.467	10.557	-10.475	9.9963	12.177	-11.000	-11.223	-10.627
10	11.48	10.562	-10.39	9.9053	12.151	-10.975	-11.241	-10.646
Mean	11.38	10.451	-10.781	10.232	12.184	-11.097	-11.244	-10.647
SD	0.0889	0.0938	0.2779	0.2187	0.128	0.123	0.21842	0.2089

Standard deviations are between 0.09 and 0.28 (cm)

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Reproducibility tests

Static state COP test

Result

Table 2. The mean and standard deviation value of four locations which measured by embedded balance measurement system

	Location1		Location2		Location3		Location4	
	X	Y	X	Y	X	Y	X	Y
1	9.919	10.062	9.941	-10.118	-9.768	10.440	-10.063	-10.230
2	9.976	10.067	10.117	-10.341	-10.404	10.623	-9.976	-10.183
3	10.063	10.250	9.936	-10.180	-10.230	10.455	-9.775	-10.105
4	10.031	10.308	10.105	-10.328	-10.201	10.401	-9.822	-10.008
5	10.061	10.248	10.101	-10.293	-10.177	10.437	-9.817	-10.025
6	10.044	10.233	9.971	-10.284	-10.196	10.457	-9.828	-10.012
7	10.056	10.258	9.907	-10.238	-10.182	10.413	-9.827	-10.010
8	10.173	10.336	10.141	-10.348	-10.188	10.451	-9.810	-10.008
9	10.259	10.367	10.128	-10.327	-10.180	10.468	-9.778	-10.114
10	10.067	10.262	9.729	-10.227	-10.194	10.410	-9.788	-10.144
Mean	10.065	10.245	10.008	-10.289	-10.171	10.450	-9.848	-10.091
SD	0.0943	0.0967	0.1337	0.0785	0.1184	0.0647	0.0945	0.0936

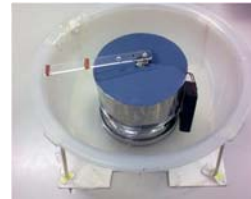
Standard deviations are between 0.06 and 0.16 (cm)

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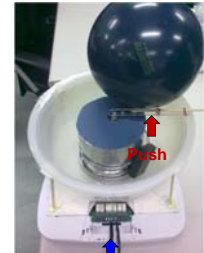
Reproducibility tests

Dynamic state COP test

The dynamic simulation device



Dynamic simulation device



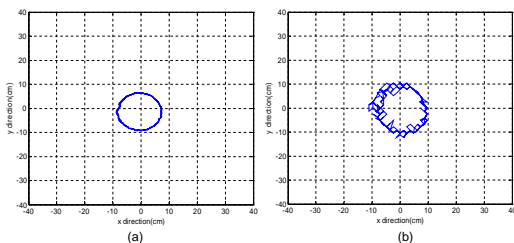
Simulation device with a ball

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Reproducibility tests

Dynamic state COP test

The regular displacement figure



High resolution balance measurement system

Embedded balance measurement system

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Reproducibility tests

Dynamic state COP test

Result

Table 3. The mean and standard deviation values of radius: R1 : Measured by the high resolution balance measurement system R2 : Measure by the embedded balance measurement system

	R1 (cm)	R2 (cm)
1	9.20	9.82
2	9.18	9.56
3	9.80	9.96
4	9.73	10.76
5	9.55	10.37
6	9.66	10.69
7	9.33	10.65
8	10.01	10.78
9	10.19	10.85
10	10.02	10.59
Mean	9.667	10.403
SD	0.353	0.459

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Balance Measure System
Human balance test

AMTI BIOMECHANICS PLATFORM



PLATFORM



Signal Processor

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Balance Measure System
Human balance test

AMTI BIOMECHANICS PLATFORM



High resolution balance measure system on the AMTI system

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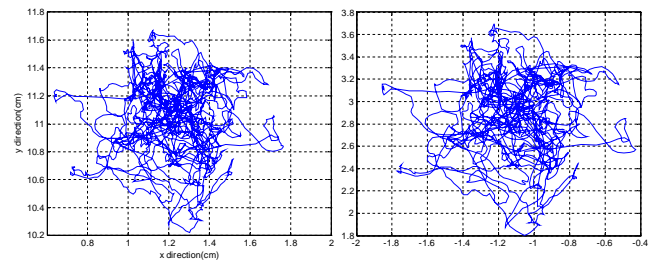
Balance Measure System
Human balance test



Subject standing on the AMTI system and our CPCMS

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Balance Measure System
Human balance test

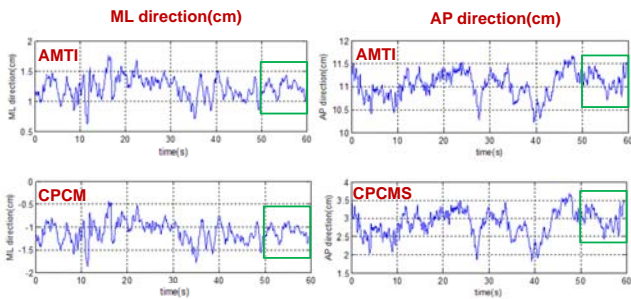


AMTI

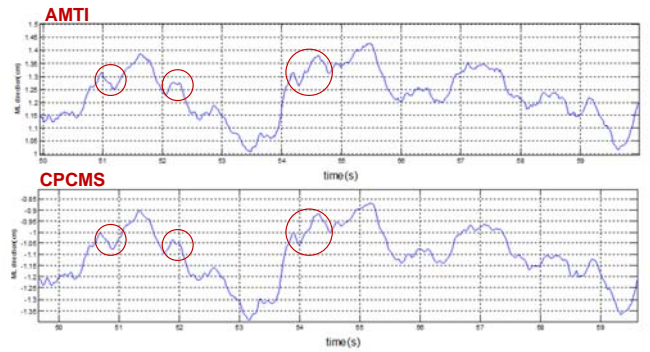
CPCMS system

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Balance Measure System
Human balance test

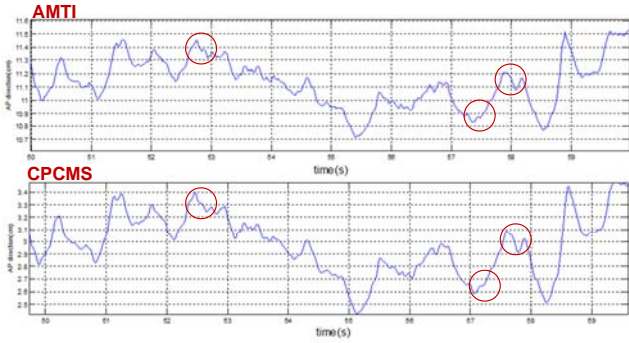


Balance Measure System
Human balance test



Balance Measure System

Human balance test



Balance Measure System

Human balance test

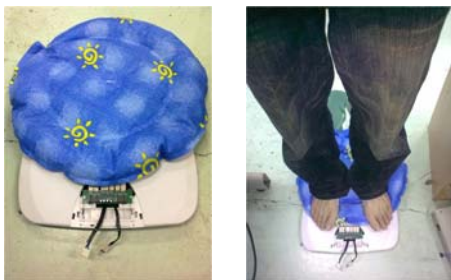
Experiment:

- (1) Standing directly on the platform:
 - Eyes open (Sway1)
 - Eyes closed (Sway2)
- (2) Standing on the platform with a soft foam (Water cushion) under their feet:
 - Eyes open (Sway3)
 - Eyes closed (Sway4)

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Balance Measure System

Human balance test



Water cushion on the balance measure system

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Balance Measure System

Human balance test

Standing directly on the platform

Standing on the platform with a soft foam (Water cushion)

Eyes open (Sway1)
Eyes closed (Sway2)

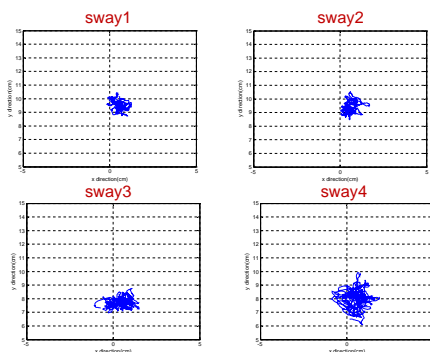
Eyes open (Sway3)
Eyes closed (Sway4)



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Balance Measure System

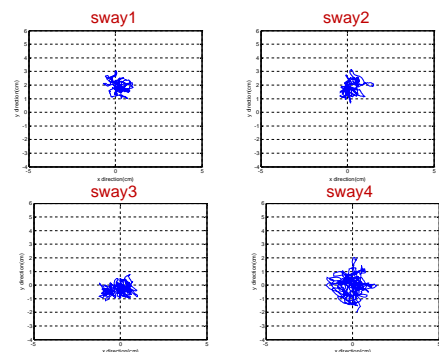
Human balance test (AMTI)



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Balance Measure System

Human balance test (Our system)



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Balance Measure System

Human balance test

Tradition Analysis method

Table1. Definition of the specific parameters examined for the postural sway

Parameters	Definition
Mean Sway (MS)	Simple mean of the distance from the mean force centre position (FCP) to all recorded force centre positions during the test.
Transversal Sway (TS)	Simple mean of the recorded x-direction values of the force centre in a coordinate system.
Sagittal Sway (SS)	Simple mean of the recorded y-direction values of the force centre in a coordinate system.
Sway Index (SI)	Relates the sway test result to human normal sway established by the manufacturer.
Sway Area (SA)	Area of the smallest polygon, which includes the total trajectory of the force centre in the horizontal plate plane.
Sway Velocity (SV)	Average travel speed of the force centre in the horizontal sway plate plane calculated by dividing the total length of the force centre trajectory (in mm) by the recording period length (in sec.).

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AMTI	Standing directly on the platform		Standing on the water cushion		P _a	P _b
	Eyes open	Eyes closed	Eyes open	Eyes closed		
MS	0.39±0.12	0.36±0.08	0.43±0.12	0.77±0.22	0.358	<0.001
TS	0.18±0.07	0.19±0.06	0.24±0.08	0.44±0.15	0.630	<0.001
SS	0.31±0.1	0.27±0.06	0.30±0.10	0.53±0.16	0.133	<0.001
MSE(X)	3.19±0.86	3.21±0.90	3.87±0.63	3.92±0.96	0.943	0.847
MSE(Y)	2.79±0.99	3.62±1.01	3.63±0.98	4.14±1.30	0.012	0.169
CPCMS						
MS	0.47±0.13	0.44±0.12	0.50±0.12	0.93±0.31	0.453	<0.001
TS	0.21±0.09	0.22±0.08	0.28±0.09	0.52±0.20	0.712	<0.001
SS	0.38±0.12	0.34±0.09	0.35±0.10	0.66±0.23	0.240	<0.001
MSE(X)	3.94±1.06	4.02±1.01	4.67±0.87	4.85±1.02	0.808	0.552
MSE(Y)	3.41±1.22	4.48±1.16	4.41±1.25	5.09±1.50	0.007	0.128

⊗ P_a: p-value for Standing directly on the platform between EO-test and EC-test.

P_b: p-value for Stand on the water cushion between EO-test and EC-test.

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Balance Measure System

Human balance test



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Volunteer Standing on the Force Platform Protected by Plastic Mats



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Acknowledgements

Yuan Ze University, Taiwan

- Intelligent System Lab. Members: UG, PG, and PHD students + Postdoctor
- Bernard C. Jiang PhD, Vice President & Department of Industrial Engineering and Management, Yuan Ze University, Taiwan

Harvard Medical School, USA

- C.K. Peng PhD, Co-Director Institute for Nonlinear Dynamics
- L. Lipsitz, MD, Chief Division of Gerontology
- V. Novak, MD, PhD, Director SAFE Laboratory

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